

Table 1 Square of natural frequency vs radial load for a simply supported circular plate

R/R^*	λ/λ^*
0	1.0000
0.1191	0.8809
0.2382	0.7618
0.3573	0.6427
0.4764	0.5236
0.5956	0.4045
0.7147	0.2854
0.8338	0.1663
0.9529	0.0471
1.0000	0

there was confusion in the definition of "the characteristic value of the frequency" and associated conclusions in the present Note. A technical comment by us (identical to the one above, by Flax) sent earlier, is due to appear in July or Aug. 1973.

To verify Southwell's theorem Eq. (1) above, one has to resort to exact closed form solutions for all elastic restraints. This is possible for a circular plate with in-plane loads. For all boundary conditions in Eq.(1), ϕ is unity. As an illustration, we quote the values for a simply supported plate in Table 1 below and the value of ϕ is unity correct to four significant figures. For a definition of the symbols, reference may be made to the comment by Flax.

Errata

Thermal Shielding by Subliming Volume Reflectors in Convective and Intense Radiative Environments

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[AIAA J. 11, 989-994 (1973)]

IN the paper, several equations are in error and may be corrected by replacing

I_0 by πI_0 in Eq. (13)

I_i by πI_i in Eq. (14)

K by πK in two terms of Eq. (17)

$n_m K_m$ by $n_m^2 \pi K_m$ in Eq. (19)

The numerical results presented in the paper are not affected by these corrections.

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Index categories: Radiation and Radiative Heat Transfer; Heat Conduction; Thermal Stresses.

Calculation of Turbulent Skin Friction on a Rotating Disk

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[AIAA J. 11, 542-543 (1973)]

THE polynomial coefficients D_5 and D_6 , Eq. (11), are incorrect. They should be

$$D_5 = -\theta \delta^+ \lambda (0.40 \lambda^2 - 5.00 \lambda + 18.70)$$

$$D_6 = 12.50 \lambda \delta^+ - \theta^2 \delta^+ \lambda (18.75 - Z.67 \lambda + 0.40 \lambda^2)$$

These changes have an insignificant effect on the calculation of circumferential skin friction and somewhat improve the calculation of wall flow direction.

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Index category: Boundary Layers and Convective Heat Transfer—Turbulent.